

1. First subroutine UEXPAN is called

a. Density and temperature dependent elastic properties are read from the .inp file, for VM9 and Zirconia, which are defined by the user. Specific heat for zirconia are also user defined.

b. If the material is "VM9" then:

i. Using Narayanswami form, ratio between relaxation time and reference (volume) relaxation time is determined as:

$$\frac{\tau_i}{\tau_{is}} = \exp \left[ -\frac{\Delta H}{R} \left( \frac{1}{T_{ref}} - \frac{x}{T} - \frac{1-x}{T_f} \right) \right]$$

where,  $\tau_i$  = structural relaxation time

$\tau_{is}$  = volume relaxation time, which is taken as 1/10<sup>th</sup> of shear relaxation times

$H$  = activation energy

$x$  = experimentally defined constant

$T_{ref}$  = reference temperature

$T$  = current temperature at end of increment

$T_f$  = fictive temperature

ii. The partial fictive temperatures  $T_{fi}(t)$ , the fictive temperature  $T_f(t)$  and the difference between fictive temperatures ( $dT_f$ ) of two sequential steps are stored as state variables and calculated as:

$$T_{fi}(t) = \frac{T_{fi}(t) + T * (\frac{\Delta t}{\tau_i})}{1 + (\frac{\Delta t}{\tau_i})}$$

where,  $\Delta t$  = time increment

$$T_f(t) = \sum c_i T_{fi}(t)$$

where,  $c_i$  are the constants defined at the reference temp  
 $dT_f = T_f - T_f(\text{previous increment})$

iii. The thermal contraction coefficients for glass and liquid states respectively, are obtained as:

$$\begin{aligned} a_g &= a_{g1} + a_{g2} * T + a_{g3} * T^2 \\ a_{gf} &= a_{g1} + a_{g2} * T_f + a_{g3} * T_f^2 \\ a_{lf} &= a_{l1} + a_{l2} * T_f + a_{l3} * T_f^2 \end{aligned}$$

Where,  $a_{g1}, a_{g2}, a_{g3}, a_{l1}, a_{l2}$  are the constants for thermal contraction coefficients in which subscript  $g$  is for glass and  $l$  for liquid state

iv. If the current temperature is greater than 600 then,

$$a_{lf} = 2.534e-05$$

else if it is less than 500 then,

$$a_{lf} = 1.082e-05.$$

v. Finally coefficient of expansion for VM9 is calculated as:

$$\text{expansion} = a_g * \text{temp. increment} + (a_{lf} - a_{gf}) * \text{fictive temp. increment}$$

c. Else if the material is "Zirconia" then:

i. If the temperature is less than 500 then,

$$a_g = 1.025e - 05$$

else if temperature is greater than 150 then,

The thermal contraction coefficient for glass is obtained as:

$$a_g = a_{g1} + a_{g2} * T + a_{g3} * T^2$$

where,  $a_{g1}, a_{g2}, a_{g3}$  are constants for thermal contraction coefficients for glass

ii. expansion =  $a_g * \text{temp.increment}$

2. After ending UEXPAN subroutine, UTRS is called to account for the temperature-time shift for a time domain viscoelastic analysis

a. As VM9 is the only viscoelastic material, Prony series for VM9 is defined by the user in the .inp file and read when required.

b.  $x$ , an experimentally defined constant, is taken as 0.27 and activation energy  $\Delta H$ , reference temperature  $T_{ref}$  along with ideal gas constant  $R$  are defined

c. Fictive temperature ( $T_f$ ) and the difference between current and previous increment fictive temperatures ( $dT_f$ ) are called from UEXPAN subroutine as statev.

d. The shift along the horizontal axis, shift factor, are determined using Tool-Narayanswamy form. The shift factor is determined at the beginning and end of the increment using:

$$\text{shift} = \exp \left[ -\frac{\Delta H}{R} \left( \frac{1}{T_{ref}} - \frac{x}{T(\dot{t})} - \frac{1-x}{T_f(\dot{t})} \right) \right]$$

where,  $T(\dot{t})$  is the temperature at any time  $\dot{t}$

$T_f(\dot{t})$  is the fictive temperature at  $\dot{t}$